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What is an EAF?

 AC or DC powered furnace which uses graphite electrodes to melt scrap iron and steel.



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A Brief History

- The Heroult company in France introduced the EAF in 1899.
- In the 1950s EAFs were small and usually located in a back comer of the melt shop.



A Brief History

- From 1965 to 1969 several primary EAF fume control systems were installed in the United States.
- The hot gases at the fourth hole caused considerable problems in the duct work. This problem with the original designs was later solved by using water-cooled ducts to reduce the temperature of the gases.





What Happens In EAF?

- Recycled steel scrap is melted and converted into high quality steel by using high-power electric arcs.
- Almost any type of metal can be used as the raw material in EAF.



Almost a third of the world's steel production today is done by EAF.



Economical Aspects

- The recovery of metal scraps benefits both the natural resources of the world and the economical growth.
- Moreover, using recycled products enables EAF to produce a variety of materials.



Electrical Power System

The modern steel plant receives low current, high voltage power from the generators of the electrical utility company. The purpose of the steel plant primary transformers is to step down this voltage. The transformers rated at 100MV soft on their store transformers are usually two steps to the process. The transformers rated at 100MV soft on their store transformer to the step down this voltage. The transformers rated at 100MV soft on their store transformers of the step down this voltage. The transformers rate is the store of the step down the voltage from high to medium levels. There are different standards but for the USA is usually as 24.5 V. Finally, a heavy duty timage transformer powers the LAF. This special furnace transformer is designed to allow the electric arc to operate within the desired current and voltage range.



Other electrical systems around the EAF are the **delta dosure**, the **power cables**, the **current conduction** arm, and the electrode holders. The power cables provide a connection between the delta closure and the current conducting arm. It is usually made of cooper wires, with a rubber water jackar around the outside for water-cooling the cables. The power cable is connected with the current conducting arm, usually made of cooper close steel or allow and or conducting arm,

 There are 3 phases used and 3 electrodes will be needed. Each of these 3 phases is connected to one of the graphite electrodes.

• Why graphite electrodes?

 They are durable at high temperatures and they have a good electrical conductivity. When the electrode is near the scrap, an ore is created and an electrical circuit is formed. To melt this scrap, there will be energy need and these arc provide the heat energy.

AA



 It is important to note that the variance in arc length is highly dependent on the EAF transformer tap voltage. Lower voltage systems (~500v) will display less variance in absolute terms than higher voltage systems (~1000v).



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Movement of Electrodes

- Vertical movement of the electrodes is obtained by adjusting the electrode arm positions.
- This phenomena controlled by the feedback from the electrical system.
- By controlling the electrical performance, we reach the predefine set point at an optimum power input.
- Electrode have an upper limit in maximum current alloved and this changes the secondary voltage parameters. The secondary voltage and arc of the lenght are directly proportional to each other.

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Furnace Operations

- Furnace charging
- Melting
- Refining
- De-slagging
- Tapping
- Furnace turn-around

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Furnace Charging

- Before the melting and heating operations start, the first step is charging into the scrap. The roof and electrods are raised and are swung to the side of the furnace allow the scrap charging to the bottom. When bucket of the furnace is full of the scrap, the roof and electrodes are lowered to strike an arc on the scrap.
- At this time electrical power is switched on and the furnace is transforming electricity to the heat the scraps. When the scraps start to melt, more volume is made available inside the furnace
- At this time the electricity is switched off and another basket will be loaded in to the furnace. The power is on again and melting of the second basket starts.

Melting

- Melting is accomplished by supllying chemical or electrical energy to the furnace interior.
- The graphide electrodes are moved downwards.
- Electrical energy is supliyed by graphite electrodes.
- Chemical energy is supplyed by lanced oxygen directly to aluminum, silicon, manganese, phosphorus, carbon and iron. All of reactions with oxygen are exothermic.
- After first charge has been melted; second charge is added into furnace.

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Refining

- Refining operations in the electric arc furnace have traditionally involved the removal of phosphorus, sulfur, aluminum, silicon, manganese and carbon from the steel.
- · Refining reactions are all dependent on the availability of oxygen.
- Higher level of P and S in the furnace charge than what is required in the in steel as per the specification, are to be removed.
- P retention in the slag depends on the bath temperature, slag basicity and FeO levels in the slag.
- reo levels in the siag.
 Removal of S in the EAT is difficult especially in the modern practice where the oxidation level of the bath is quite high.
 At the end of refining, bath temperature measurement and bath sample are taken. If the temperature is too low, power can be applied to the bath. Low temperature adjustment is carried out in the ladle fumace.

De-Slagging

- Some of the undesirable materials within the bath are oxidized and enter the slag phase. De-slagging operations are carried out to remove these impurities from the furnace.
- It is advantageous to remove as much phosphorus into the slag as early in the heat as possible
- During slag foaming operations, carbon may be injected into the slag where it will reduce FeO to metallic iron and in the process produce carbon monoxide which helps foam the slag. If the high phosphorus slag has not been removed prior to this operation, phosphorus reversion will occur. During slag foaming, slag may overflow the sill level in the EAF and flow out of the slag door.

| The following | ng table | shows t | the typical | constituents | of a | n EAF slag: | |
|-----------------------------------|----------|---------|-------------|--------------|------|-------------|--|
| | | | | | | | |

| Component | Source | Composition Range |
|------------------|--------------------------|-------------------|
| cio | Charged | 40 - 60 % |
| SiO ₂ | Oxidation product | 5 - 15 % |
| feD | Oxidation product | 10 - 30 % |
| MgO | Charged as dolomite | 3 - 8 % |
| Caf, | Charged - slag fluidizer | |
| MnO | Oxidation product | 2 - 5% |
| s | Absorbed from steel | |
| p | Oxidation product | |

Tapping

- Once the desired steel composition and temperature are achieved in
- the furnace, the tap-hole is opened, the furnace is tilted, and the steel

pours into a ladle for transfer to the next batch operation.

- · De-oxidizers may be added to the steel to lower the oxygen content prior to further processing.
- This is commonly referred to as "blocking the heat" or "killing the steel".

Tapping

- Common de-oxidizers ===> > Al or Si (in the form of ferrosilicon or silicomanganese)
- Most carbon steel operations aim for minimal slag carry-over.
- For ladle furnace operations, a calcium aluminate slag is a good choice for sulfur control.

Tapping

- Slag forming <u>compounds</u> ===>> ladle at tap, a slag cover is formed prior to transfer to the ladle furnace.
- If the slag cover is <u>insufficient</u> ===>> more slag materials may be added.

Furnace Turn-around

- What is the furnace turn-around ?
- Period following completion of tapping until the furnace is recharged for the next heat.
- How it works ?
- Electrodes and roof are raised and the furnace lining is inspected for refractory damage.

Furnace Turn-around

- In most modern furnaces, the increased use of water-cooled panels has reduced the amount of patching or "fettling" required between heats.
- Furnace turn-around time is generally the largest dead time period in the tap-to-tap cycle.

| | Engineer | ing Steel | | | | |
|-----------------------------------|----------|-----------|----|-------|-------|--|
| SIMULATION | Element | Result | | Min | Max | |
| Steel University | C* | 0.000 | 00 | j 0.3 | 0.43 | |
| · | SI* | 0.000 | 0 | 0 | 0.5 | |
| | Mn* | 0.000 | 00 | j 0.6 | 0.9 | |
| | P | 0.000 | 0 | 0 | 0.03 | |
| 1-Engineering Steel is chosen. | S* | 0.000 | 0 | 0 | 0.04 | |
| 2-Target composition $ ightarrow$ | Cr | 0.000 | 0 | 0 | 1.2 | |
| | Mo | 0.000 | 0 | 0 | 0.3 | |
| | N | 0.000 | 0 | 0 | 0.3 | |
| | Cu | 0.000 | 0 | 0 | 0.35 | |
| | N* | 0.000 | 0 | 0 | 0.005 | |
| | Nb. | 0.000 | 0 | 0 | 0.01 | |
| | n | 0.000 | 0 | 0 | 0.01 | |
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| | | | | | | |

Target steel grade:

Raw Material's Composition

| Material 💌 | c% • | Si% • | Mn% 🚽 | P% - | s% - | Cr% 💌 | Mo% • | N6% * | Cu% 🔹 | Sn% - | №Ь% - | Ti% 💌 |
|----------------------|-------|-------|-------|-------|--------|-------|-------|-------|-------|-------|-------|-------|
| Direct Reduction Fe | 2,4 | 0 | 0 | 0,1 | 0,01 | 0 | 0 | 0 | 0 | | 0,03 | 0,02 |
| Shredded | 0,03 | 0,015 | 0 | 0,02 | 0,03 | 0,12 | 0,02 | 0,1 | 0,16 | 0,013 | | |
| Heavy 2 | 0,03 | 0,022 | 0 | 0,028 | 0,035 | 0,26 | 0,03 | 0,18 | 0,18 | | | |
| Heavy 1 | 0,025 | 0,017 | 0 | 0,025 | 0,033 | 0,2 | 0,03 | 0,15 | 0,18 | | | |
| Turnings | 0 | 0 | 0 | 0,03 | 0,113 | 0,698 | 0,538 | 0 | 0 | | | |
| Bundles 2 | 0,04 | 0,016 | 0,12 | 0,01 | 0,006 | 0,032 | 0 | 0,02 | 0,018 | | | 0,001 |
| Bundles 1 | 0,027 | 0,012 | 0,12 | 0,01 | 0,006 | 0,032 | 0 | 0,02 | 0,018 | | | 0,001 |
| Internal Low Alloyed | 0,17 | 0,04 | 0,31 | 0,013 | 0,0014 | 0,26 | 0,14 | 0,4 | 0,02 | | | 0,015 |
| Plate and Structural | 0,25 | 0,25 | 1 | 0,025 | 0,025 | 0,15 | 0,05 | 0,15 | 0 | | | 0 |
| EAF Dust | 0 | 0,91 | 4,44 | 0,019 | 0,001 | 20,03 | 0 | 11,2 | 0 | | | 0,003 |

| | | | | | | | Target ster | l orade: | | | |
|-----------------------|----------|-------------------|-----|------------------|------------------|----------|----------------|-------------|-------------|-------------|-----------|
| Kaw Material | UNK COST | Mass | | | Volume | CON | Engineeri | n Steel | | | |
| No1 Heavy | \$1004 | \odot | 5 | 0 | 6m ³ | \$ 000 | | -pene | | | |
| No2 Heavy | \$1408 | | 0 | | Om ³ | 50 | Element | Result | | Min | Max |
| | | | | - | | | C* | 0.360 | 0 | 0.3 | 0.43 |
| Internal Low Alkyed | \$2408 | $\mathbf{\nabla}$ | 0 | $\mathbf{\circ}$ | Om ³ | 50 | 81* | 0.172 | 0 | • | 0.5 |
| Plate and Structural | \$2908 | \odot | 16 | | Ore ³ | \$4640 | Mini | 0.676 | 0 | 0.6 | 0.9 |
| Red Duration | | - | | Ä | (m) | | P | 0.000 | 0 | 0 | 0.03 |
| NOT BUTURS | 610UN | V | | w. | 000- | | 81 | 0.025 | 0 | 0 | 0.04 |
| No2 Bundles | \$170t | | 1 | 0 | 1m ³ | \$170 | Cr | 0.144 | 0 | 0 | 1.2 |
| Direct Reduced Iron | \$2208 | | 2 | 0 | 100 | 5440 | Mo | 0.040 | 0 | • | 0.3 |
| | | | | - | | | N | 0.133 | 0 | 0 | 0.3 |
| Shredded | \$2004 | $\mathbf{\nabla}$ | 0 | \circ | Om ³ | 80 | 04 | 0.009 | 0 | ۰ | 0.35 |
| Turnings | \$1108 | \odot | 0 | 0 | 0m ³ | 50 | N ^e | 0.000 | 0 | 0 | 0.005 |
| 717.4-4 | F (778) | - | | Ä | ~ | | ND | 0.002 | 0 | ٥ | 0.01 |
| Ener Was | Pien | 0 | | w. | | | Π | 0.002 | 0 | 0 | 0.01 |
| Total | | | 241 | | tóm ¹ | \$6050 | Clivicates | elements th | at any ingr | tially) ram | ovable in |
| Cost per metric tonne | | | | | | \$254 /t | the subsects | theorem for | ry steeling | king sime | lation |

1st Trial

| | Please select y | our steel g | rade and compose your scrap | selection. | | | | | | | |
|-------|----------------------|-------------|-----------------------------|------------------|---------|----------------|----------|---------|-----|-------|---|
| and a | Raw Material | Unit cost | Mass | Volume | Cost | Target stee | l grade: | | | | 0 |
| riai | Not Heavy | 836M | | 100 | 8 160 | Ergineer | ng Steel | | | | |
| | | | | | | Dement | Result | | Min | Max | |
| | No2 Heavy | \$1451 | | 5003 | \$140 | C* | 0.408 | 0 | 0.3 | 0.43 | |
| | Internal Low Alloyed | \$2454 | | (im) | \$240 | 81 | 0.195 | 0 | 0 | 0.5 | |
| | Plate and Structural | \$2901 | | 17m ² | \$9570 | Mn* | 0.789 | 0 | 0.6 | 0.9 | |
| | | | | | | | 0.030 | \odot | ٥ | 0.03 | |
| | No1 Dundes | \$1024 | | 1103 | \$180 | 81 | 0.022 | 0 | 0 | 0.04 | |
| | No2 Dundes | \$1758 | 2 | 2m ³ | \$340 | œ | 0.135 | 0 | 0 | 1.2 | |
| | Direct Destand lines | | | 201 | | Mo | 0.043 | \odot | ٥ | 0.3 | |
| | CIRCLE REAL PERIOD | 02231 | | 200 | 4000 | N | 0.135 | 0 | 0 | 0.3 | |
| | Stredded | \$2054 | | 0m ³ | 80 | Cu . | 0.011 | 0 | 0 | 0.35 | |
| | Turnings | \$1154 | | (im) | 50 | N ² | 0.000 | 0 | 0 | 0.005 | |
| | | | | | | ND | 0.003 | 0 | 0 | 0.01 | |
| | EAF dust | \$-1204 | | Que, | \$0 | n | 0.002 | 0 | 0 | 0.01 | |
| | Total | | 411 | 2007 | \$11510 | | | | | | |

Cost







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Melting & Slagging

-Electrodes should not be broken so speed is important.

-Sample is taken for control before slagging.

-For slagging, air(30 kg/min) and C(50 Nm³/min) is blown.

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| | Additives |
|---|---------------------------------------------------------------------------------------|
| - | We need C and Mn |
| - | To reach target composition, we added 10 kg Ferro manganese as additivies |

| Element | Current | | Min | Max |
|---------|---------|---|--------|--------|
| c | 0.29808 | 0 | 0.3000 | 0.4300 |
| 9 | 0.14578 | • | | 0.5000 |
| Mn | 0.58594 | 0 | 0.6000 | 0.9000 |
| P | 0.00873 | 0 | | 0.0000 |
| 8 | 0.02268 | • | | 0.0400 |
| Cr | 0.49455 | • | | 1.2000 |
| ~ | | | | |
| | | 0 | | 0.0050 |
| N | 0.29100 | • | | 0.3000 |
| ND | 0.00218 | • | | 0.0100 |
| n | 0.00150 | • | | 0.0100 |
| | | | | |

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Final Composition

| Liquid Steel | Composition / wt% | | | |
|--------------|-------------------|---|--------|--------|
| Element | Current | | Min | Max |
| c | 0.30047 | 0 | 0.3000 | 0.4300 |
| 8 | 0.14731 | 0 | | 0.5000 |
| Mn | 0.00403 | • | 0.6000 | 0.9000 |
| P | 0.02464 | 0 | | 0.0300 |
| 5 | 0.02268 | • | | 0.0400 |
| Cr. | 0.49735 | 0 | | 1,2000 |
| A | | | | |
| 8 | | 0 | | 0.0050 |
| N | 0.28970 | 0 | | 0.3000 |
| ND | 0.00215 | 0 | | 0.0100 |
| n | 0.00150 | 0 | | 0.0100 |
| v | 0.00146 | 0 | | 0.0100 |
| No | 0.07411 | 0 | | 0.3000 |

Conclusion

| | | | Target |
|--------------------------|----------------------------|---|--------------|
| Total time | 0H:55M | 0 | 1H:30M |
| Tap temperature | 1678 °C | 0 | 1655-1685 °C |
| Liquid Steel Composition | A | 0 | |
| Tapping mass /kg | 50218 Avg | | |
| Electrical energy | 24331 kWh (\$485 kWh/t) | | |
| Power | \$13869 | | |
| Scrap | \$10970 | | |
| Additions | \$5 | | |
| Other consumables | \$227 | | |
| Total cost | \$25071 (\$499.25.1) | | |
| | | | |

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THANK YOU

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