

BLAST FURNACE

060110410 CEREN YAĞŞI
 060110405 DILAY KİBAROĞLU
 060120549 ÖZGE NUR ÜNLÜ
 060120516 OSMAN ÇAĞLAR BAYSALLI
 060100913 NERGİZ ALIYEVA
 060110406 BİRSEN BAŞ
 060120503 BERİL SAADET YENİGÜL
 060140707 ELİF ÖZKAN
 060100306 MUSTAFA ÖZDEMİR
 060130712 ANIL ÜZER

INTRODUCTION TO BLAST FURNACE

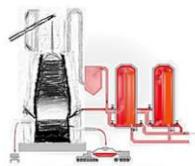
* THE PURPOSE OF A BLAST FURNACE IS TO CHEMICALLY REDUCE AND PHYSICALLY CONVERT IRON OXIDES INTO LIQUID IRON CALLED HOT METAL. THIS PARTICULAR PROCESS IS THE DOMINATING IRONMAKING ROUTE FOR PROVIDING THE RAW MATERIALS FOR STEELMAKING.

ZONES OF THE BLAST FURNACE

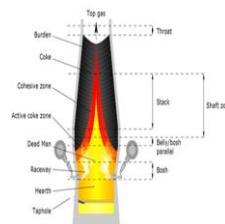
Main Components



Auxiliar Equipment



ZONES OF BLAST FURNACE MAIN COMPONENTS



THROAT: THE BURDEN SURFACE AT THE TOP OF THE BLAST FURNACE

SHAFT: WHERE THE ORES ARE HEATED AND REDUCTION REACTIONS START

BELLY OR BOSH PARALLEL: THE SHORT VERTICAL SECTION

BOSH: THE ORE REDUCTION COMPLETES, AND THE ORES ARE MELTING DOWN

HEARTH: WHERE THE MOLTEN MATERIALS ARE COLLECTED AND TAPPED VIA THE TAP-HOLES

ZONES OF BLAST FURNACE MAIN COMPONENTS



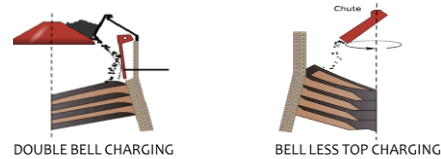
SCHEMATIC VIEW OF TUYERES
AND BUSTLE PIPE

TUYERES AND BUSTLE PIPE:
THE BUSTLE PIPE IS A LARGE DIAMETER DOUGHNUT SHAPE PIPE ENCIRCLING THE FURNACE. IT FEEDS HOT AIR TO THE TUYERES THE TEMPERATURES OF THE HOT BLAST RANGE FROM 900 °C TO 1250 °C.

ZONES OF BLAST FURNACE AUXILIAR COMPONENTS

CHARGING SYSTEM

THE MATERIALS USUALLY HELD IN HOPPERS AT THE TOP OF THE FURNACE UNTIL A CHARGE, USUALLY CONSISTING OF SOME TYPE OF METALLIC, COKE AND FLUX HAVE ACCUMULATED. THE PRECISE FILLING ORDER IS DEVELOPED BY THE BLAST FURNACE OPERATORS CAREFULLY CONTROL GAS FLOW AND CHEMICAL REACTIONS INSIDE THE FURNACE.



DOUBLE BELL CHARGING

BELL LESS TOP CHARGING

ZONES OF BLAST FURNACE AUXILIAR COMPONENTS

HOPPERS: FOR TEMPORARILY STORING THESE RAW MATERIALS

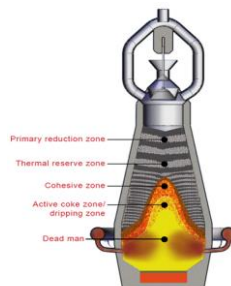
BELT CONVEYORS: FOR TRANSPORTING RAW MATERIALS TO THE FURNACE TOP

BF-TOP PRESSURE RECOVERY TRIBUNE: A BF USUALLY OPERATED WITH A FURNACE TOP PRESSURE OF ABOUT 250 KPA. THE RECOVER THE ENERGY FROM THE LARGE VOLUME OF HIGH PRESSURE EXHAUST GAS, THE BF IS EQUIPPED, AFTER DUST REMOVAL, WITH TOP PRESSURE RECOVERY TRIBUNE (TRT) FOR GENERATING ELECTRIC POWER BY UTILIZING THE PRESSURE DIFFERENCES BETWEEN THE FURNACE TOP AND GAS STORING HOLDER.

DUST REMOVAL: EQUIPMENT FOR DUST REMOVAL AND RECOVERY.

CASTHOUSE: WHERE THE MOLDEN IRON AND REMAINING SLAG SEPERATED BEFORE THE IRON IS PURED INTO TORPEDO CAR OR LADLE FOR TRANSPORT TO FURTHER REFINEMENT.

ZONES OF BLAST FURNACE

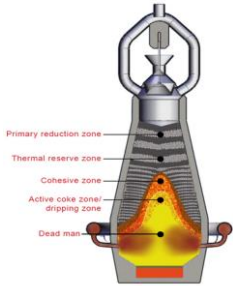


PRIMARY REDUCTION ZONE:
THE UPPER PART OF SHAFT, WHERE HIGHER VALENCY IRON OXIDES ARE REDUCED. TEMPERATURE RANGES FROM 400 °C TO 1000 °C

THERMAL RESERVE ZONE:
THE LOWER PART OF THE SHAFT ZONE, WHERE THE TEMPERATURE IS MAINTAINED AT ABOUT 1000-1200 °C. IN THIS ZONE, REDUCTION OF WUSTITE TO METALLIC IRON TAKES PLACE

COHESIVE ZONE:
EXTENDS FROM ABOVE BOSH NEAR THE WALL UP TO MIDDLE PART OF STACK IN THE CENTER OF THE BF. THE MATERIALS HAS REACHED ABOUT 1200 °C START TO SOFT EN AND MELT EXCEPT COKE PARTICLES

ZONES OF BLAST FURNACE



ACTIVE COKE ZONE:

BENEATH THE COHESIVE ZONE, WHERE THE FINAL REDUCTION TO METALLIC IRON COMPLETES, MELTS OF SLAG AND HOT METAL FROM AND DRIP THROUGH THE COKE LAYER

DEAD MAN:

A POROUS PACKED-BED OF UNREACTED COKE PARTICLES SITTING OR FLOATING IN THE HEARTH. CARBURIZATION OF HOT METAL TAKE PLACE WITHIN THE DEAD MAN

CHEMICAL REACTIONS

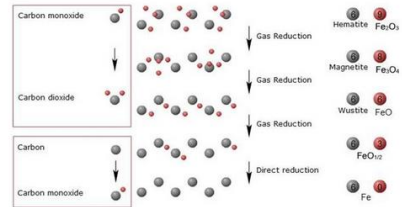
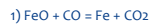


ILLUSTRATION FOR PROCESS OF CONVERTING FROM HEMATITE TO METALLIC IRON

CHEMICAL REACTIONS DIRECT REDUCTION



DIRECT REDUCTION USES CARBON AS THE REDUCTANT AND GENERATES EXTRA CO GAS; DIRECT REDUCTION COSTS A LOT OF ENERGY

CHEMICAL REACTIONS INDIRECT REDUCTION

IT IS ALSO CALLED GAS REDUCTION. GAS REDUCTION TAKES PLACE BETWEEN THE CO OF H_2 WITH SOLID BURDEN MATERIALS OF IRON OXIDES. IT REMOVES ABOUT $\frac{2}{3}$ OF THE TOTAL OXYGEN IN THE IRON ORE. THE INDIRECT REDUCTION REACTIONS WITH CO ARE;



PULVERIZED COAL INJECTION

- THE INJECTION OF AUXILIARY REDUCTANTS SUCH AS COAL, OIL AND NATURAL GAS IS USED TO LOWER THE COST OF HOT METAL. COAL IS THE MOST COMMONLY USED AND ALLOWS COST SAVINGS AND HIGHER BLAST TEMPERATURES. COAL INJECTION LEADS TO INCREASED PRODUCTIVITY FROM USING OXYGEN ENRICHED BLAST
- COAL INJECTION IS CATEGORISED BY THEIR VOLATILE MATTER CONTENT 6-12% IS CLASSIFIED AS LOW VOLATILE, 12-30% AS MID VOLATILE AND OVER 30% AS HIGH VOLATILE COAL

HOT METAL PRETREATMENT

THE PROCESS IN WHICH IMPURITIES ARE REMOVED FROM THE HOT METAL BEFORE BOS ARE CALLED HOT METAL PRETREATMENT, AT PRESENT, AN INTEGRATED PROCESS OF SMELTING IN THE BF, HOT METAL PRETREATMENT, DECARBURIZING IN THE BOS, AND THE SECONDARY REFINING HAS BECOME THE STANDART MANUFACTURING PROCESS FOR HIGH GRADE STEELS.

HOT METAL PRETREATMENT

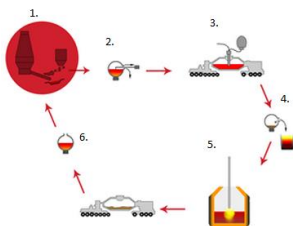
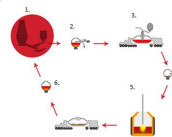


ILLUSTRATION FOR HOT METAL PRETREATMENT

HOT METAL PRETREATMENT



1.DESILICONIZATION: IS THEREFORE CONDUCTED AS A PRETREATMENT PROCESS BY ADDING IRON OXIDES SUCH AS MILL SCALE AND SINTERED ORE FINES TO HOT METAL IN THE RUNNERS IN THE CASTHOUSE OF THE BF OR IN THE TRANSFER VESSEL

2.SLAG SEPERATION

3.DEPHOSPHORIZATION: IS USUALLY CARRIED OUT AFTER DESILICONIZATION REACTION PROCEEDS MORE QUICKLY AT LOWER SILICON CONTENTS.

4.SLAG SEPERATION

5.DECARBURIZATION

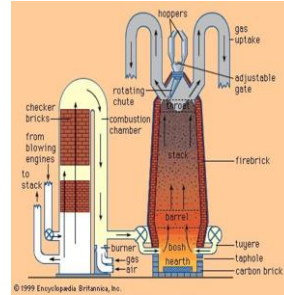
6.SLAG RECYCLING

RAW MATERIAL

ORE AND COKE; TO PRODUCE ONE TONNE OF HOT METAL A TOTAL OF ABOUT 1,600 IRON BEARING AS SINTERED ORE, LUMP ORE AND PELLETS ARE REQUIRED AND IT CONSUMES ABOUT 380 KG OF COKE AS THE REDUCTANT. THE ORE AND COKE ARE CHARGED IN ALTERNATE LAYERS FROM THE TOP OF THE BF.



HOT BLAST



APPROXIMATELY 1000 Nm³/tonne HOT METAL OF HOT BLAST IS ALSO BLOWN THROUGH THE TUYERES AFTER PREHEATING TO 1150- 1250 °C AT THE HOT STOVES. THE HUMIDITY AND THE OXYGEN CONCENTRATION OF THE HOT BLAST ARE ALSO CONTROLLED.

SINTERING AND COLD STRENGTH

SINTER IS A METHOD OF FUSING IRON ORE FINES INTO THE PARTICLES SUITABLE FOR CHARGING INTO THE BLAST FURNACE. THE LIME (CaCO₃, CaO) IN THE SINTER IS ADDED AS A FLUX TO THE BLAST FURNACE AND SINTER IS CATEGORIZED. MEAN SINTER SIZES RANGE FROM 15 TO 25 MM AT THE SINTER PLANT.

COLD STRENGTH

LOW COLD STRENGTH RESULTS IN A HIGH FINES RATE.

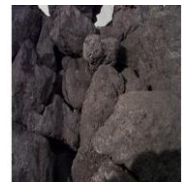
MELTING PROPERTIES AND COKE

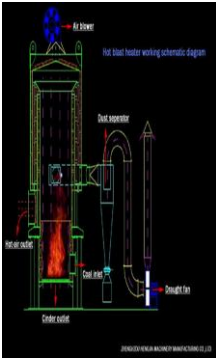
MELTING PROPERTIES

THE MELTING OF SINTER IS DETERMINED BY THE CHEMICAL COMPOSITION. SINTER START SOFTENING AND MELTING AT 1200-1250 °C. VERY BASIC SINTER MELTS AT HIGHER TEMPERATURES OF 1300 C AND IF THE FeO CONTENT IS VERY LOW , MELTING TEMPERATURES CAN EXCEED 1500 °C.

COKE

SINCE THE 18TH CENTURY COKE HAS BEEN AS THE MOST IMPORTANT CARBON SOURCE IN THE BF PROCESS. SINCE THE 1960'S PART OF THE COKE USED HAS BEEN REPLACED BY AUXILIARY REDUCTANTS INJECTED THROUGH THE TUYERES SUCH AS OIL, TAR, COAL AND NATURAL GAS .





- THE AIR BLOW INTO THE BLAST FURNACE IS PRE-HEATED TO 100-1250 °C IN THE HOT BLAST STOVES. THE STOVES WORK IN CYCLES, FIRST THE REFRACTORY BRICKS IN STOVE ARE HEATED BY BURNERS USING BF GAS. THEN THE COLD BLAST BLOWN IN AND THE HEAT STORED IN THE BRICKS IS TRANSFERRED TO THE GAS. THE HOT BLAST IS DELIVERED TO THE BF VIA A HOT BLAST MAIN, BUSTLE PIPE AND THE TUYERES.
- AT THE TOP OF THE FURNACE THE BLAST FURNACE GAS IS HOT AND CONTAINS A LARGE AMOUNT OF FINE PARTICLES. TO REMOVE THESE, THE GAS IS LEAD VIA DOWNCOMER TO A DUST CATCHER AND WET CLEANING SYSTEM.

OUTPUTS

- SLAG IS FORMED THE GANGUE MATERIALS OF THE BURDEN AND THE ASHES OF THE COKE AND OTHER AUXILIARY REDUCTANTS. DURING BF PROCESS, PRIMARY SLAG DEVELOPS TO A FINAL SLAG.
- FOR MAIN COMPONENTS; SILICON DIOXIDE, CALCIUM OXIDE, MAGNESIUM OXIDE AND ALUMINUM OXIDE MAKE UP ABOUT 96% OF THE SLAG.
- THE MINOR COMPONENTS ARE MAGNESIUM OXIDE, TITANIUM DIOXIDE, POTASIUM OXIDE, SODIUM OXIDE, SULFUR AND PHOSPHORUS.

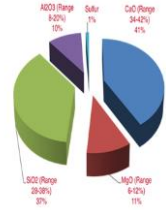
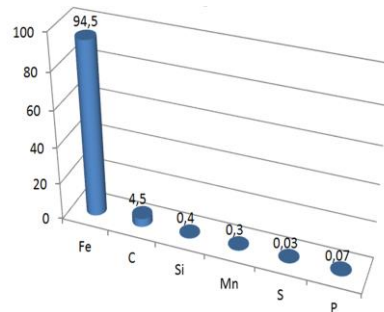


Table: Chemical Composition of Hot Metal

HOT METAL IS THE MAIN PRODUCT OF THE BF PROCESS. IT IS CARBON SATURATED IRON WITH A NUMBER OF IMPURITIES SUCH AS SILICON, MANGENESE, SULFUR AND PHOSPHOROUS. IT IS TAPPED FROM THE BF HEARTH AT A TEMPERATURE BETWEEN 1480-1520 °C. A TYPICAL COMPISITION OF HOT METAL CAN BE SEEN IN THE TABLE.

Element	Symbol	Typical (wt%)
Iron	Fe	94.5
Carbon	C	4.5
Silicon	Si	0.40
Manganese	Mn	0.30
Sulfur	S	0.03
Phosphorus	P	0.07



THE REDUCTION OF IRON ORE BY CARBON AND HYDROGEN GASES IS A VERY COMPLICATED PROCESS. FOR A BETTER UNDERSTANDING OF THE FACTORS INFLUENCING THE REDUCIBILITY OF THE ORES, SINTERS AND PELLETS, HERE IS A VERY SIMPLIFIED VIEW OF RATE-CONTROLLING REACTIONS. IN MOST CASES, THE IRON ORE IS IN THE HEMATITE FORM AND REDUCTION STARTS FROM HEMATITE AND PROCEED IN THE FOLLOWING ORDERS;

HEMATITE→MAGNETITE→WUSTITE→METALLIC IRON



WHEN THE COKE AND HEMATITE IS HEATED AND REACTS WITH CARBON MONOXIDE, IT IS TRANSFORM TO MAGNETITE. CARBONDIOXIDE AND WATER WHICH EVAPORATES INSTANTLY.

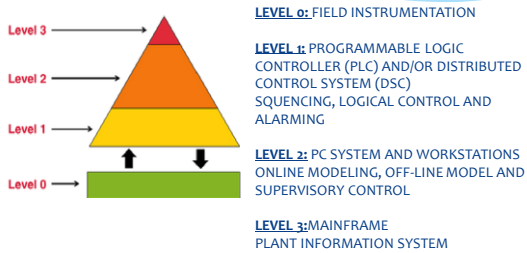


MAGNETITE TURNS INTO WUSTITE.



WUSTITE TURNS INTO METALLIC IRON

CONTROL ARCHITECTURE LAYOUT



BLOWING IN PROCESS

THE PROCESS OF STARTING A BLAST FURNACE IS CALLED BLOWING IN AND IS MADE UP OF SEVERAL STEPS:

- 1) DRYING
- 2) FILLING
- 3) LIGHTING

BLOWING OUT PROCEDURE

- 1) DURING BLOWING DOWN THE FURNACE IS OPERATED WITHOUT CHARGING UNTIL THE BURDEN LEVEL REACHES APP. THE TUYERE LEVEL.
- 2) WATER SPREYS ARE INSTALLED AT THE TOP OF THE FURNACE TO CONTROL THE TOP GAS TEMPERATURE AND ONE OR MORE LEVELS OF STEAM SPRAYS ARE INSTALLED ON LOWER LEVELS FOR COOLING AND MAINTAINM THE PRESSURE.
- 3) THE STEAM SPRAYS ARE ACTIVATED WHEN THE BURDEN LEVEL HAS PASSED.
- 4) THE BLAST RATE AND TEMPERATURE REDUCED AS THE BURDEN LEVEL LOWERS TO CONTROL THE TOP GAS TEMPERATURE AND ITS OXYGEN AND HYDROGEN CONTENT.
- 5) FINALLY DRAINING THE SALAMANDER. THE SALAMANDER IS THE IRON PRESENT IN THE HEART BELOW THE TOP HOLES AND IS USUALLY DRAINIED. IF PERMITTED TO SOLIDIFY, BLASTING IS REQUIRED TO REMOVE THE CHUNK OF SOLID IRON. THE SALAMANDER IS TAPPED THROUHT A HOLE IN THE BRICKWORK OF THE FURNACE BOTTOM CREATED BY DRILLING AND THE LAST PART WITH AN OXYGEN LANCE.

IRREGULARITIES OPERTATION

DURING BLAST FURNACE OPERATION IRREGULARITIES CAN OCCUR; CAUSING CONSIDERABLE CONCERN AND CAN LEAD TO SERIOUS TROUBLE IF NOT HANDLED CORRECTLY. THE MOST COMMON IRREGULATIES OCCURING ARE:

- 1) SLIP
- 2) SCAFFOLDING
- 3) CAHNNELING

STEEL UNIVERSITY

FUEL AND FLUX

Sinter (77.06%)

A: 45000

Pellets (16.61%)

A: 9000
B: 697

Lump Ores (0.48%)

A: 3000
B: 198

Revert (0.85%)

A: 500

Total mass: 81999 kg
Total cost: 15660

Fuel

Coke 1: 3000, Coke 2: 5500, Coke 3: 4200
Coal 1: 1400, Coal 2: 1300, Coal 3: 2000

Flux

Limestone: 1900, Dolomite: 2400
Silica: 2000, Olivine: 606

OTHER PROPERTIES

Process settings

Working volume (m³): 2700
Type of pig iron: (batches per hour): 10

Temperatures (°C)

Hot metal: 1430
Ambient: 25
Top gas: 260
Ore: 60

Hot Blast Properties

Temperature (°C): 1150
Pressure (kPa): 130
Temperature drop (°C): 45.4
Humidity (g/Nm³): 12.5

Gas Additions (%)

Oxygen enrichment: 4
C to CH₄ ratio: 1
H₂: 45
Direct reduction rate: 45

OUTGOING COMPOSITION

Outgoing Compositions

Hot metal	Slag	Slag Basicity	Yield
Fe: 94.85	FeO: 1.02	R2: 1.131	1HM/year: 297815.73
C: 3.60	CaO: 39.61	R3: 1.584	1HM/day: 8585.19
Si: 1.10	SiO ₂ : 35.02	R4: 1.278	1HM/batch: 35.77
Mn: 0.29	Al ₂ O ₃ : 8.51		
Ti: 0.01	MgO: 15.06		
V: 0.00	MnO: 1.05		
S: 0.02	V ₂ O ₅ : 0.00		
P: 0.12	TiO ₂ : 0.14		
T (°C): 1513	CaF ₂ : 0.00		
	P: 0.00		
	S: 0.03		

Top gas	Costs
CO ₂ : 31.56	Oxygen: 2.36
CO: 20.87	Blast: 4.76
N ₂ : 47.72	Humidity: 0.06
H ₂ : -0.71	Top Gas: -28.29
CH ₄ : 0.57	Hot Blast: 7.30
	Burden: 441.74
	Total Cost: 427.83

HEAT AND MASS BALANCE

Heat and Mass Balance Results			
Mass In			
Mixed ore	1630.17kg / 1HM	47.39%	
Coke	351.44kg / 1HM	10.32%	
Small coke	0.00kg / 1HM	0.00%	
Coal powder	125.09kg / 1HM	3.69%	
Lump coal	0.00kg / 1HM	0.00%	
Flux	153.58kg / 1HM	5.73%	
Blast	1624.54kg / 1HM	50.70%	
Free water	8.13kg / 1HM	0.24%	
Total	3337.83kg / 1HM	98.27%	
Heat In			
Carbon oxidation	7943078kg / 1HM	81.50%	
Hot blast	1306078kg / 1HM	13.43%	
Hydrogen oxidation	107802kg / 1HM	1.11%	
Slag forming	120257kg / 1HM	1.29%	
Materials heat	201144kg / 1HM	2.09%	
Total	9747348kg / 1HM	100.00%	
Mass Out			
Hot Metal	1000.00kg / 1HM	30.76%	
Slag	358.00kg / 1HM	11.03%	
Top gas	1620.75kg / 1HM	50.01%	
Dust	56.24kg / 1HM	0.47%	
Moisture	15.33kg / 1HM	1.73%	
Total	3250.31kg / 1HM	100.00%	
Heat Out			
Oxide decomposition	7274162kg / 1HM	74.63%	
Carbonate decomposition	136809kg / 1HM	1.40%	
Moisture decomposition	155540kg / 1HM	1.64%	
Free water evaporation	16752kg / 1HM	0.17%	
Coal decomposition	4052kg / 1HM	0.04%	
Million sec	983227kg / 1HM	10.09%	


CHARGING RESULTS



Charging Results	
Blast Furnace Volume:	2700 m ³
Blast furnace utilization coefficient:	3.18. It is very good!
Coke rate is:	344.41 kg / 1HM. It is very good!
Coal rate is:	120.69 kg / 1HM.
Fuel rate is:	474.1 kg / 1HM. It is very good!
The blast temperature is:	1105 °C.
Fe content in ores is:	59.89%. It is very good!
Energy utilization coefficient is:	92.07%. It is very good!
Carbon energy utilization coefficient is:	72.53%. It is very good!
Mass balance error:	2.58%. This is higher than 2%. Please try to decrease it.
Total cost:	1427.93 \$ / 1HM

ORE

Blast Furnace Simulation



Ore

Sinter (80.50%)

A

Pellets (13.60%)

A

B

Lump Ores (5.72%)

A

B

Revert (0.16%)

A

Total mass 50000 kg
Total cost 16230

FUEL AND FLUX

Fuel

Coke 1 Coke 2 Coke 3

Coal 1 Coal 2 Coal 3

Flux

Limestone Dolomite

Silica Olivine

OTHER PROPERTIES

Type of pig iron:
 Steel Foundry

Target (Composition)

Target Si content (%)

Target slag basicity

Process settings

Working volume (m³)

Type of pig iron: (batches per hour)

Temperatures (°C)

Hot metal

Top gas

Ambient

One

Gas Additions (%)

Oxygen enrichment H₂

C to CH₄ ratio Direct reduction rate

Hot Blast Properties

Temperature (°C) Temperature drop (°C)

Pressure (kPa) Humidity (g/m³)

Heat Loss Model

Free Heat Loss Flood Heat Loss

Heat loss (%)

OUTGOING COMPOSITION

Outgoing Compositions

Hot metal	Slag	Slag Basicity	Yield
Fe: 94.07	FeO: 0.00	R2: 1.132	1 tHM / year: 2842100.58
C: 3.40	CaO: 40.35	R3: 1.529	1 tHM / day: 8100.30
Si: 1.10	SiO2: 35.65	R4: 1.225	1 tHM / batch: 34.16
Mn: 0.30	Al2O3: 8.85		
Ti: 0.01	MgO: 14.15		
V: 0.00	MnO: 1.04		
S: 0.02	V2O5: 0.00	CO2: 26.67	Oxygen: 2.19
P: 0.10	TiO2: 0.13	CO: 23.00	Blast: 5.86
T (°C): 1783	CaF2: 0.00	N2: 50.43	Humidity: 0.07
	P: 0.00	H2: -27.76	Top Gas: -27.76
	S: 0.67	CH4: 0.53	Hot Blast: 1.00
			Burden: 473.62
			Total Cost: 463.98

HEAT AND MASS BALANCE

Outgoing Compositions

Heat and Mass Balance Results

Mass In	Mass Out
Blast iron: 4833.00kg / 1 tHM 43.84%	Hot Blast: 100.00kg / 1 tHM 28.21%
Coke: 414.20kg / 1 tHM 11.22%	Slag: 288.10kg / 1 tHM 10.41%
Small coke: 0.00kg / 1 tHM 0.00%	Top gas: 2101.24kg / 1 tHM 89.28%
Coal powder: 101.10kg / 1 tHM 2.80%	Dust: 57.61kg / 1 tHM 0.47%
Lump coal: 0.00kg / 1 tHM 0.00%	Moisture: 10.00kg / 1 tHM 1.83%
Flux: 190.11kg / 1 tHM 0.37%	Total: 3544.97kg / 1 tHM 100.00%
Blow: 1201.30kg / 1 tHM 34.90%	
Free water: 0.30kg / 1 tHM 0.02%	
Total: 2614.67kg / 1 tHM 88.26%	

Heat In	Heat Out
Carbon oxidation: 8320.02kg / 1 tHM 78.88%	Oxide decomposition: 7270401kg / 1 tHM 88.61%
Hot blast: 1913106kg / 1 tHM 18.47%	Carbonate decomposition: 147000kg / 1 tHM 1.35%
Hydrogen oxidation: 120000kg / 1 tHM 1.24%	Moisture decomposition: 188770kg / 1 tHM 1.59%
Slag heating: 122117kg / 1 tHM 1.17%	Free water evaporation: 17000kg / 1 tHM 0.71%
Molecular heat: 273400kg / 1 tHM 2.81%	Coal decomposition: -4030kg / 1 tHM -0.50%
Total: 10427407kg / 1 tHM 100.00%	Molten iron: 1170900kg / 1 tHM 11.24%
	Slag: 82220kg / 1 tHM 4.80%
	Top gas: 823300kg / 1 tHM 5.61%

CHARGING RESULTS



Outgoing Compositions

Heat and Mass Balance Results

Charging Results

Blast Furnace Volume: 2700 m³

Blast furnace utilization coefficient: 3.04. It is very good!

Coke rate is: 405.91 kg / 1 tHM.

Coal rate is: 101.13 kg / 1 tHM.

Fuel rate is: 507.04 kg / 1 tHM.

The blast temperature is: 1105 °C.

Fe content in ores is: 59.79%. It is very good!

Energy utilization coefficient is: 88.87%.

Carbon energy utilization coefficient is: 67.66%. It is very good!

Total cost 482.98 \$ / 1 tHM

REFERENCES

- Moore, Colin London : Institute of Metals, 1991
- Lee, Peter L. editor London : Springer London, 1993
- Westwood, N.J., U.S.A. Waste materials used in concrete manufacturing. Noyes Publications, c1997
- A reference book for blast furnace operators .Wegmann, Eu. F Moskow : Mir Pub., c1984
- Blast furnace phenomena and modeling. London : Elsevier Applied Science, c1987
- Coke reactivity and its effect on blast furnace operation. Warrendale, PA : Iron and Steel Society, c1990
- Coke Oven Techniques . The Commission of the European Communities Directorate-General Energy. Author Dordrecht : Springer Netherlands, 1982
- Yüksek fırın prosesi. Biswas, Anil K. Zonguldak : Ereğli Demir-Çelik Fabrikaları A. Ş., [1991]